

## Determination of equation of state parameters of poly(dimethylsiloxane)–benzene system by intrinsic viscosity

Ayten Kuntman\*

Faculty of Electrical and Electronic Engineering, Technical University of Istanbul,  
80626, Maslak – Istanbul, Turkey

and Ferdane Yılmaz

Department of Chemistry, Yıldız University, 80270, Şişli – Istanbul, Turkey  
(Received 19 July 1994; revised 7 September 1994)

The equation of state exchange energy ( $X_{12}$ ) and entropy ( $Q_{12}$ ) parameters and the ratio of contact sites ( $s_2/s_1$ ) of the poly(dimethylsiloxane)–benzene system were determined using equation of state theory and intrinsic viscosity measurements. The values of  $X_{12}$  and  $Q_{12}$  parameters for  $s_2/s_1 = 0.67$  are found to be  $16.64 \text{ J cm}^{-3}$  and  $-0.0394 \text{ J cm}^{-3} \text{ K}^{-1}$ , respectively.

(Keywords: thermodynamics; equation of state; intrinsic viscosity)

### Introduction

The thermodynamics of many solvent–solvent and polymer–solvent pairs have been investigated by Flory and his collaborators using equation of state theory<sup>1–8</sup>. Three quantities,  $X_{12}$ ,  $Q_{12}$  and  $s_2/s_1$ , were introduced in this theory. The parameters  $X_{12}$ ,  $Q_{12}$  and  $s_2/s_1$  are defined as the interchange energy upon formation of contacts between unlike molecules, the entropy erasing from interchange of neighbouring molecules, and the ratio of surface areas (or contact sites) for a polymer segment and solvent molecule, respectively.

The values of  $X_{12}$  and  $Q_{12}$  (especially  $Q_{12}$ ) were chosen arbitrarily to fit the theory and experimental results by Flory and co-workers. The ratio of  $s_2/s_1$  was estimated with either an approximation, where the solvent may be represented by a sphere whose volume is equal to the characteristic molar volume of the solvent  $V_1^*$  and the solute by a cylinder of volume  $V_1^*$ , or the sum of the surface areas of constituent groups given by Bondi<sup>9</sup>.

Recently, a simple procedure based on intrinsic viscosity measurements has been proposed to estimate parameters  $X_{12}$  and  $Q_{12}$  of poly(4-chlorostyrene) in various solvents<sup>10</sup>. This procedure was developed to calculate the value of  $s_2/s_1$  in our previous papers<sup>11,12</sup>.  $Q_{12}$ ,  $X_{12}$  and  $s_2/s_1$  were calculated for poly(ethyl methacrylate)–isopropyl alcohol and polystyrene–cyclohexane mixture using the above-mentioned method<sup>11,12</sup>. It was shown that the results obtained by this procedure are in good agreement with literature values for the polystyrene–cyclohexane system<sup>7</sup>.

In this study, the values of  $X_{12}$ ,  $Q_{12}$  and  $s_2/s_1$  for poly(dimethylsiloxane) solution in benzene were estimated using the equation of state theory from intrinsic viscosity measurements. Polymer–solvent interaction

parameters ( $\chi_1$ ,  $\chi_2$ ) were determined as a function of temperature from equation of state theory. Our results are compared with the result obtained from osmotic pressure experiments<sup>8</sup>.

### Theoretical background

The relation between intrinsic viscosity and molecular dimensions of a polymer chain in a solution is given by the following equations<sup>13</sup>:

$$\alpha_\eta^3 = \frac{[\eta]}{[\eta]_\theta} \quad (1)$$

$$K_\theta = \Phi \langle r^2 \rangle_0 / M^{3/2} \quad (2)$$

$$\langle r^2 \rangle_0 = ([\eta]_\theta M / \Phi)^{2/3} \quad (3)$$

$$K_\theta = [\eta]_\theta / M^{1/2} \quad (4)$$

The symbols in these equations are defined as follows:  $\alpha_\eta^3$  is the expansion factor;  $[\eta]_\theta$  and  $[\eta]$  are intrinsic viscosities at, respectively, theta and ordinary temperatures;  $K_\theta$  is the unperturbed chain dimension constant;  $M$  is the molecular weight of polymer;  $\langle r^2 \rangle_0$  is the mean square end-to-end distance of the unperturbed coil;  $\Phi$  is the universal viscosity constant (Flory–Fox constant) for the polymer chain and has a value of  $2.5 \times 10^{21} \text{ mol}^{-1}$  if the intrinsic viscosity unit is  $\text{dl g}^{-1}$ .

$\alpha_\eta^3$  is a function of the excluded volume parameter ( $z$ ). The excluded volume parameter is related to the polymer–solvent interaction density ( $B$ ), as given by:

$$\alpha_\eta^3 = 1 + kz \quad (5)$$

$$z = (3/2\pi)^{3/2} (B\Phi/K_\theta) M^{1/2} \quad (6)$$

$$B = \bar{v}^2(1 - 2\chi_1)/V_1 N_A \quad (7)$$

where  $k$  is a constant with a value of 1.05–1.55 (ref. 14),  $\bar{v}$  is the specific volume of polymer,  $\chi_1$  is the thermodynamic interaction parameter in infinitely dilute polymer solutions,  $V_1$  is the molar volume of the solvent,  $N_A$  is Avogadro's number. The empirical relation in

\*To whom correspondence should be addressed at: Department of Electrical and Electronic Engineering, Istanbul University, 34850 Avcılar, Istanbul, Turkey

equation (5) is the best fit to the experimental data over the range  $0 < \alpha_n^3 < 1.6$  (ref. 14).

In this study, equations (1)–(7) were rearranged in the following form:

$$\chi_1 = 0.5 - \{(\alpha_n^3 - 1)V_1 N_A [\eta]_\theta / \Phi M \bar{v}^2 2k(3/2\pi)^{3/2}\} \quad (8)$$

If we say that

$$S = N_A / \Phi 2k(3/2\pi)^{3/2} \quad (9)$$

then a simple equation is obtained for calculation of  $\chi_1$ :

$$\chi_1 = 0.5 - \{(\alpha_n^3 - 1)[\eta]_\theta S V_1 / \bar{v}^2 M\} \quad (10)$$

Polymer–solvent interaction parameter,  $\chi$ , is a function of concentration and temperature.  $\chi$  can be expanded in series with respect to volume fraction of polymer,  $v_2$ , at constant temperature<sup>15</sup>:

$$\chi = \chi_1 + \chi_2 v_2 + \chi_3 v_2^2 + \dots \quad (11)$$

where  $\chi_1$ ,  $\chi_2$ ,  $\chi_3$ , are the thermodynamic interaction parameters which are functions of temperature. The volume fraction of polymeric samples approaches zero at very dilute solutions. Therefore  $\chi$  can be taken as equal to  $\chi_1$  with a good approximation. In this study, as the intrinsic viscosities were measured at very low concentrations,  $\chi_1$ , which was calculated using equation (10), was assumed to be equal to  $\chi_1$  in equation (11).

In the equation of state theory, polymer–solvent interaction parameters are given by<sup>15</sup>:

$$\lim_{v_2 \rightarrow 0} \chi = \chi_1 = (p_1^* V_1^* / \bar{v}_1 R T) [A^2 \alpha_1 T/2 + Y_{12}] - V_1^* Q_{12} (s_2/s_1)^2 / R \quad (12)$$

$$\begin{aligned} \chi_2 = & \{2(1 - s_2/s_1)(Y_{12} + Z_{12} T) \\ & + [2Y_{12} + (1 - p_2^* T_2^* / p_1^* T_1^*) A] A \alpha_1 T \\ & - (3 + 2\alpha_1 T + 2\alpha_1^2 T^2)(2\alpha_1 T A^3/9)\} (p_1^* V_1^* / \bar{v}_1 R T) \end{aligned} \quad (13)$$

where

$$A = (1 - T_1^* / T_2^*)(p_2^* / p_1^*) - (s_2/s_1) X_{12} / p_1^* \quad (14)$$

$$Y_{12} = X_{12} (s_2/s_1)^2 / p_1^* \quad (15)$$

$$Z_{12} = -Q_{12} (s_2/s_1)^2 \bar{v}_1 / p_1^* \quad (16)$$

Quantities appearing in these equations are defined as follows:  $V_1^*$ ,  $p_1^*$  and  $T_1^*$  are, respectively, the characteristic molar volume, pressure and temperature of the solvent;  $p_2^*$  and  $T_2^*$  are the corresponding quantities for the polymer;  $R$  is the universal gas constant;  $\alpha_1$  is the thermal expansion coefficient of the solvent;  $\bar{v}_1 = (V_1/V_1^*)$  is the reduced volume;  $s_2/s_1$  is the ratio of surface areas for a polymer segment and solvent molecule;  $X_{12}$  and  $Q_{12}$  are the exchange energy and entropy parameters of interaction, respectively. As shown in refs 10–12, if equation (12) is rearranged, a straight line equation is obtained which is given by the following equations for its slope ( $sl$ ) and intercept ( $I$ ):

$$sl = (s_2/s_1)^2 V_1^* X_{12} / \bar{v}_1 R \quad (17)$$

$$I = p_1^* V_1^* \alpha_1 A^2 / 2 \bar{v}_1 R - Q_{12} (s_2/s_1)^2 V_1^* / R \quad (18)$$

### Experimental

A sample of poly(dimethylsiloxane) (PDMS), having a viscosity-average molecular weight of about  $2.8 \times 10^4$ , was obtained from the Petrarch System Inc., Bristol, USA. A home-made modified Ubbelohde-type capillary viscometer was used for intrinsic viscosity measurements. The viscometer was immersed in a constant temperature bath controlled to  $\pm 0.02^\circ\text{C}$ .

Intrinsic viscosities were calculated using the following relationship:

$$[\eta] = \lim_{c \rightarrow 0} (\eta_{sp}/c) \quad (19)$$

Polymer solutions were obtained in the viscometer by successive dilution of the initial PDMS solution. Intrinsic viscosity values were obtained by least-squares linear fitting of the experimental data. Detailed experimental procedures for viscometric measurements and calculations are given in ref. 16.

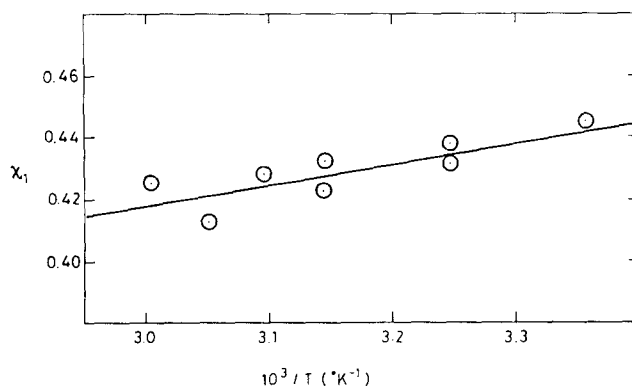
### Results and discussion

The intrinsic viscosities of PDMS solution in benzene were performed in the temperature range of about  $25$ – $60^\circ\text{C}$ . The intrinsic viscosity results of PDMS are given in Table 1. Thermal expansion factors,  $\alpha_n$ , were determined by equation (1). In this calculation,  $[\eta]_\theta$  was obtained as  $0.132 \text{ dl g}^{-1}$  from the  $K_\theta$  value of methyl ethyl ketone by means of equation (4)<sup>17</sup>. Thermodynamic interaction parameters ( $\chi_1$ ) of PDMS in benzene were calculated from equations (1) and (10) by using the intrinsic viscosity data at the temperatures measured. The variation of  $\chi_1$  with reciprocal values of absolute temperature is shown in Figure 1.

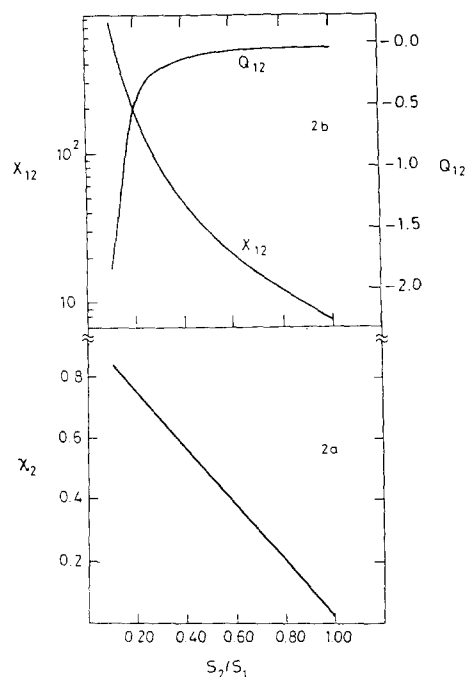
By use of equations (12)–(16) and from the slope and intercept of Figure 1, a number of curves at various conditions have been simulated. The value of equation

**Table 1** Intrinsic viscosity values for poly(dimethylsiloxane)–benzene mixtures at various temperatures

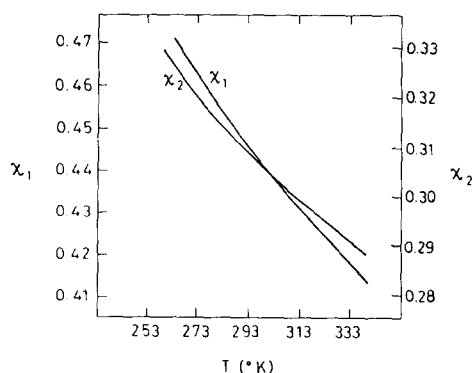
$T$ ( $^\circ\text{C}$ )	25	35	45	50	55	60
$[\eta]$	0.179	0.184 0.189	0.189 0.196	0.192	0.205	0.193



**Figure 1** Polymer–solvent interaction parameter  $\chi_1$  obtained from experimental measurement results of intrinsic viscosity for the PDMS–benzene plotted against reciprocal values of absolute temperature



**Figure 2** (a) Variation of  $\chi_2$  with the ratio  $s_2/s_1$  at the theta point for the PDMS-benzene system. (b) Variation of  $X_{12}$  (left ordinate) and  $Q_{12}$  (right ordinate) with the ratio  $s_2/s_1$  at the theta point for the PDMS-benzene system



**Figure 3** Value of  $\chi_1$  (left ordinate) and  $\chi_2$  (right ordinate), calculated according to the equation of state theory, plotted as functions of temperature for the PDMS-benzene system. In this calculation values of  $X_{12}$ ,  $Q_{12}$  and  $s_2/s_1$  were taken as  $16.64 \text{ J cm}^{-3}$ ,  $-0.0394 \text{ J cm}^{-3} \text{ K}^{-1}$  and 0.67, respectively

of state exchange energy ( $X_{12}$ ) and entropy ( $Q_{12}$ ) parameters and the ratio of  $s_2/s_1$  for the PDMS-benzene system were calculated. Values of parameters used for calculation for the PDMS-benzene system were taken as,  $V_1^* = 95.84 \text{ cm}^3 \text{ mol}^{-1}$ ,  $T_1^* = 4709 \text{ K}$ ,  $T_2^* = 5528 \text{ K}$ ,  $\alpha_1 = 1.223 \times 10^{-3} \text{ K}^{-1}$ ,  $\bar{v}_1 = 1.2917$ ,  $p_1^* = 628 \text{ J cm}^{-3}$ ,  $p_2^* = 341 \text{ J cm}^{-3}$ , at  $25^\circ\text{C}$  (ref. 18). As discussed in the previous papers<sup>5,11,12</sup>, it was shown that the equation of state contribution of  $\chi_1$  is insensitive to the ratio  $s_2/s_1$ , but  $\chi_2$  is sensitive to this ratio. In this study, the theta point ( $-7^\circ\text{C}$ ) was taken as reference to perform these calculations<sup>19</sup>. It is known that theoretical and experimental values of  $\chi_2$  are in the order of  $1/3$  at the theta point<sup>15</sup>.

The variation of  $\chi_2$ ,  $X_{12}$  and  $Q_{12}$  values with  $s_2/s_1$  ratios at the theta point is shown in Figure 2. If one applies our procedure, it is apparent from Figure 2a that the most suitable value of  $s_2/s_1$  should be between 0.6

and 0.7 for  $\chi_2 \approx 1/3$ . The values of segment surface areas for polymer segment and solvent molecule have been calculated in a previous paper<sup>8</sup> as 0.598 and 0.877 for the PDMS-benzene system. As mentioned in the Introduction, these values are found from the approximation that the solvent may be represented by a sphere and the solute by a cylinder and also from the sum of the surface areas of constituent groups given by Bondi<sup>9</sup>. As can be seen from Figure 2a, the values obtained for  $\chi_2$  are 0.387 and 0.136 for the  $s_2/s_1$  values of 0.598 and 0.877, respectively, while the theory predicts that  $\chi_2 \approx 1/3$  at the theta point. For  $s_2/s_1 = 0.757$  (the value used in ref. 8), which is between the values chosen arbitrarily by Flory's group,  $\chi_2$  is 0.260. In our procedure, we obtained  $s_2/s_1 = 0.67$  from the theoretical value of  $\chi_2 = 1/3$  for the PDMS-benzene pair. So, this procedure gives reasonable values of  $s_2/s_1$ , being close to the former value in the above-mentioned calculation procedures.

The equation of state exchange energy and entropy parameter values for  $s_2/s_1 = 0.67$  are found to be  $16.64 \text{ J cm}^{-3}$  and  $-0.0394 \text{ J cm}^{-3} \text{ K}^{-1}$ , respectively, for the PDMS-benzene system in this study. These values are comparable with the  $X_{12}$  and  $Q_{12}$  values given as  $22 \text{ J cm}^{-3}$  and  $-0.04 \text{ J cm}^{-3} \text{ K}^{-1}$ , respectively, by Flory and Shih<sup>8</sup>. The lower  $X_{12}$  value indicates better solubility. On the other hand, the positive  $Q_{12}$  value shows that the solubility as well as the entropy of the mixture increase with temperature, or vice versa. The solubility of a mixture is determined by the magnitude of the effective exchange energy parameter,  $\bar{X}_{12}$  defined as  $\bar{X}_{12} = \bar{v}TQ_{12}$ , where  $\bar{v}$  is the reduced volume of the mixture and  $T$  is the absolute temperature. So, if the effective exchange energy parameter,  $\bar{X}_{12}$ , is low enough, the mixture is miscible.

Finally, by using the obtained values of  $Q_{12}$ ,  $X_{12}$  and  $s_2/s_1$ , values of  $\chi_1$  and  $\chi_2$  were calculated according to the equation of state theory and plotted as functions of temperature in Figure 3 for the system PDMS-benzene. Both of them decrease with temperature.

## References

- 1 Flory, P. J., Eichinger, B. E. and Orwoll, R. A. *Macromolecules* 1968, **1**, 287
- 2 Eichinger, B. E. and Flory, P. J. *Trans. Faraday Soc.* 1968, **64**, 2035
- 3 Eichinger, B. E. and Flory, P. J. *Trans. Faraday Soc.* 1968, **64**, 2053
- 4 Flory, P. J. *Discuss. Faraday Soc.* 1970, **49**, 7
- 5 Flory, P. J. and Höcker, H. *Trans. Faraday Soc.* 1971, **67**, 2258
- 6 Höcker, H. and Flory, P. J. *Trans. Faraday Soc.* 1971, **67**, 2270
- 7 Höcker, H., Shih, H. and Flory, P. J. *Trans. Faraday Soc.* 1971, **67**, 2275
- 8 Flory, P. J. and Shih, H. *Macromolecules* 1972, **5**, 761
- 9 Bondi, A. J. *Phys. Chem.* 1964, **68**, 441
- 10 Yilmaz, F. and Baysal, B. M. *Polym. Int.* 1993, **31**, 107
- 11 Kuntman, A. and Baysal, B. M. *Polymer* 1993, **34**, 3723
- 12 Kuntman, A., Uyanik, N. and Baysal, B. M. *Polymer* 1994, **35**, 3356
- 13 Flory, P. J. 'Principles of Polymer Chemistry', Cornell University Press, Ithaca, 1953
- 14 Yamakawa, H. 'Modern Theory of Polymer Solutions', Harper and Row, New York, 1971, p. 384
- 15 Erman, B. and Flory, P. J. *Macromolecules* 1986, **19**, 2342
- 16 Kuntman, A. PhD thesis, Technical University of Istanbul, Institute of Science and Technology, 1989
- 17 Flory, P. J., Mandelkern, L., Kinsinger, J. B. and Schulz, W. B. *J. Am. Chem. Soc.* 1952, **74**, 3364
- 18 Shih, H. and Flory, P. J. *Macromolecules* 1972, **5**, 758
- 19 Kuwahara, N. T., Miyake, M., Kaneko, J. and Fruchi, J. *Rep. Progr. Polim. Phys. Japan* 1962, **5**, 1